

COUPLING OF ELECTROMAGNETIC WAVES AND SPACE CHARGE WAVES
IN TYPE "O" TRAVELING WAVE TUBES

P. Ricci

Translation of "L'Accoppiamento delle Onde Elettromagnetiche e delle Onde di Carica Spaziale nei Tubi ad Onde Viaggianti Tipo 'O'", XII Convegno Internazionale delle Comunicazioni, Genova, 8-12 October 1964, Vol. 2, p. 1001-1015.

(NASA-TM-75249) COUPLING OF ELECTROMAGNETIC
WAVES AND SPACE CHARGE WAVES IN TYPE O
TRAVELING WAVE TUBES (National Aeronautics
and Space Administration) 18 p HC A02/MF
A01

N78-18309
Unclas
CSCL 09C G3/33 05389



NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
WASHINGTON, D.C. 20546

FEBRUARY, 1978

STANDARD TITLE PAGE

1 Report No NASA-TM-75249	2 Government Accession No	3 Recipient's Catalog No	
4 Title and Subtitle COUPLING OF ELECTROMAGNETIC WAVES AND SPACE CHARGE WAVES IN TYPE "O" TRAVELING WAVE TUBES		5 Report Date February 1978	
		6 Performing Organization Code	
7 Author(s) P. Ricci		8 Performing Organization Report No	
		10 Work Unit No	
9 Performing Organization Name and Address Leo Kanner Associates, Redwood City, California 94063		11 Contract or Grant No NASw-2790	
		13 Type of Report and Period Covered Translation	
12 Sponsoring Agency Name and Address National Aeronautics and Space Administration, Washington, DC 20546		14 Sponsoring Agency Code	
15 Supplementary Notes Translation of "L'Accoppiamento delle Onde Elettromagnetiche e delle Onde di Carica Spaziale nei Tubi ad Onde Viaggianti Tipo "O", XII Convegno Internazionale delle Comunicazioni, Genova, 8-12 October 1964, Vol. 2, p. 1001-1015			
16 Abstract H. Derfler has observed that a parameter defined by Pierce's perturbation method does not have the same physical significance as an analogous parameter described by a differently derived equation of W. Kleen. A modification of Pierce's method is proposed, which yields an equation of Derfler's type, and also allows quicker and easier calculation of a given traveling wave tube's parameters.			
17 Key Words (Selected by Author(s))		18 Distribution Statement Unclassified - Unlimited	
19 Security Classif (of this report) Unclassified	20 Security Classif (of this page) Unclassified	21 No. of Pages	22 Price

COUPLING OF ELECTROMAGNETIC WAVES AND SPACE CHARGE WAVES IN TYPE "O" TRAVELING WAVE TUBES

P. Ricci

Summary

The first section of this paper gives a brief presenta- /1001*
tion of the electromagnetic problem connected with traveling
wave tubes, with special reference to J.R. Pierce's classic
works on the subject, and discussing the fourth-degree equation
this author developed to calculate gain in these tubes. Then an
observation made by H. Derfler at the International Congress on
Microwave Tubes at Paris, 1956, is noted, according to this obser-
vation, a parameter defined by Pierce's equation does not have
the same physical significance as an analogous parameter defined
by an equation developed in a different manner by W. Kleen, even
though this latter may be written in such a way as to be formally
identical to that of Pierce. To verify this fact, Derfler calcu-
lated the electromagnetic field in a radially symmetrical travel-
ing wave tube (one of the few cases which can be approached
analytically by the direct route). The author got a resulting
equation for calculating gain in the tube which, while still of
the fourth degree, could be considered a combination of Pierce's
and Kleen's two equations. In subsequent sections a modification
of Pierce's perturbation method is proposed. This new form yields
an equation of the same type as Derfler's, yet also (more impor-
tantly) allows quicker and easier calculation of the parameters
of a given traveling wave tube. Then the physical significance
of our calculation is discussed, and finally, to confirm our
theory, the formulas developed are specialized for the radially
symmetrical case studied by Derfler, obtaining in this case the

* Numbers in the margin indicate pagination in the foreign text.

same results as he did.

1. The Electromagnetic Problem of a Traveling Wave Tube

Type "O" traveling wave tubes consist basically (cf. Fig. 1) of a periodic structure and an electron beam, suitably accelerated and focused by means of an electron gun. The beam is under the influence of a very intense static magnetic field /1002 which prevents scattering in the transverse direction. The theory of interaction between the kinetic energy of the particles and the electromagnetic energy of the wave supported by the periodic structure may be developed under the following simplifying hypotheses

- 1) High frequency signals are quite small.
- 2) They possess a dependency on z (axial direction of the beam) of the type $e^{-\sqrt{z}}$.
- 3) There are no positive ions.
- 4) The beam does not achieve relativistic speeds.

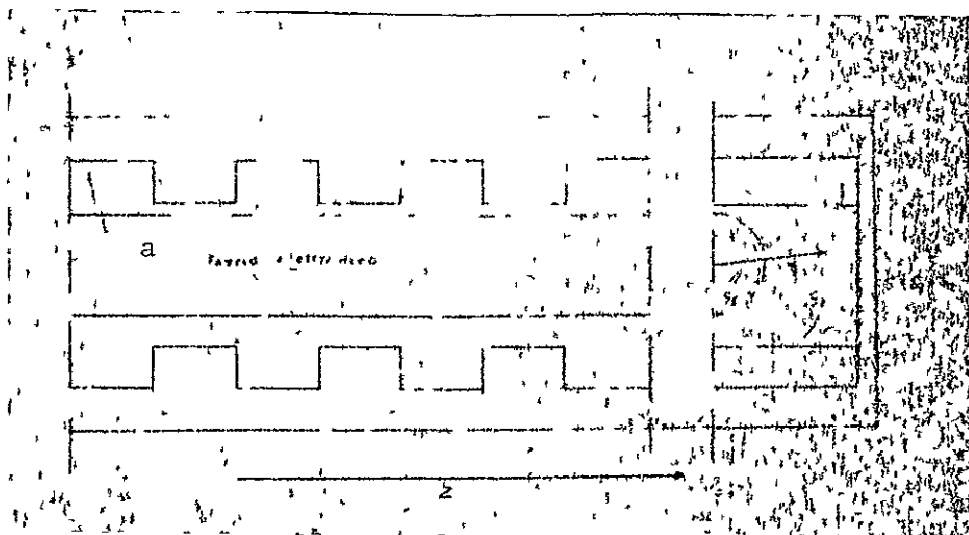


Fig. 1. Example of periodic electron guide

Key: a. Electron beam

5) The axial magnetic field mentioned above is intense enough to prevent transverse motion (with respect to z) of the particles. One may also assume that at an initial time the electrons all leave the electron gun at the same speed u_0 . Now, if the plasma pulsation is defined as

$$\omega_p = \sqrt{\frac{\rho_0 e}{m \epsilon_0}}$$

where

/1003

- ρ = density of charge of the beam at exit from the electron gun
- $\frac{e}{m}$ = η = ratio between charge and mass of the electron
- ϵ_0 = dielectric constant of vacuum

then, by calculating the current density as a function of the longitudinal component E_z of the electric field (cf. [7] p. 183-84), one easily finds that the beam can be considered as a medium with a tensorial dielectric constant given by

$$\epsilon = \begin{vmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 + \frac{\omega_p^2}{(j\omega - \Gamma u_0)} \end{vmatrix} \quad (2)$$

From Eq. 2 one also finds that the TM modes are the only ones capable of feeling the effects of the beam. In fact, given that the particles can vibrate only in the longitudinal direction, only the longitudinal component of the electric field can modulate the beam and draw from it the necessary energy to amplify signals.

By introducing Eq. 2 into Maxwell's equations, one finds that the TM modes mentioned above (cf. for instance [7] p. 166) can be derived from a vector potential.

$$A = T(r) e^{-\Gamma z} \underline{z}_0 \quad (3)$$

where $\underline{z}_0$ is the versor of the z-axis solution of the homogeneous equation

$$\nabla^2 T - (k^2 - \Gamma^2) \left(1 + \frac{\omega_p^2}{j\omega(\omega - \omega_0)^2} \right) T = 0 \quad (4)$$

Thus the problem of determining the field in a structure /1004 containing an electron beam becomes one of the beam's contours. This problem is not too complex in the case in which the structure supporting the electromagnetic waves is a continuous structure of the type of a normal wave guide. The problem is also easily solved using Birdsall and Whinnery's charts [2]. In fact, the constant Γ may be found, with the continuity of the tangential fields E_z and H_t imposed on the beam contour, by the equation

$$\left(\frac{H_t}{E_z} \right)^i = Y(r) = \left(\frac{H_t}{E_z} \right)^e \quad (5)$$

where the indices i and e indicate, respectively, internal and external quantities of the beam, and in the case of continuous structures one may set [2]

$$Y(r) = Y\left(\frac{\omega}{\mu_0}\right) = Y(\beta_0) \quad (6)$$

Having this quantity at our disposal, the problem can be immediately solved with the aforementioned charts. The constant thus determined corresponds to the propagation constant of so-called space charge waves (waves which exist only in the presence of the space charge of the beam). In continuous-structure tubes these waves are the only waves with a velocity lower than that of light. But the case is different for traveling wave tubes in which the structure surrounding the beam is of a periodic type. This structure propagates waves with phase velocities slower than that of light even in the absence of the electron beam ("cold" case). Furthermore, to obtain maximum signal amplification, the beam is given a velocity u_0 close to that of one of the slow supported waves in the cold case (synchronous wave). Thus Y^e has a pole [2] for $r = r_m^0 = J\beta e$, such that Eq. 6 cannot be set up in this case, furthermore, it is not easy to impose the contour conditions on the periodic structure. Because of /1005 this, a direct solution of the problem generally turns out to be very complicated. An appropriate solution, however, can be obtained in this case by using the perturbation method.

We owe this method to the works of Pierce [1] and Wainstein [5]. It consists essentially of the perturbation of the cold solution ($\omega_p = 0$ throughout the structure) in such a way as to obtain the serial development of the transcendental equation (approximating Eq. 5) for the Y^e poles. Thus one can remove from the sum the term $r = r_m^0$ relative to the pole, by writing it separately, and replace r in the other terms with the quantity $J\beta e$, which does not differ greatly from T in analogy to what was done in writing Eq. 6. Thus Eq. 5 is approximated with a fourth-degree equation. In this equation there appears a variable term $\sim r^2$ in which the factor is a parameter generally indicated by Q and called the space charge parameter. This parameter, however, despite its name, does not take account of the phenomena due expressly to the modulation of the space charge. This has been

noted elsewhere by H. Derfler [4], who calculated, in order to test such an assertion, the field in a circular guide periodically loaded with thin discs and crossed by an electron beam concentric with it. He found that to Pierce's parameter Q there is added a term due to the space charge waves. In fact, the structure in the presence of the beam is conceptually different from the cold structure; suffice it to consider that (Eq. 4) for each eigenvalue k_T of the problem there are 4 waves, instead of the two that generally result in homogeneous problems (two of these waves correspond to the direct and inverse ones in the absence of the beam, and the other two are space charge waves introduced by the beam, having phase velocities close to $\underline{u}_0$).

2. The Modified Perturbation Method

We thus want to reconsider the perturbation method to include space charge phenomena as well. To this end we will first perturb the cold solution, then we will consider the effect of modulation of the space charge by perturbing the space charge /1006 waves in a guide with perfectly conductive walls (in which there are no slow waves in the absence of the beam). By combining the two cases we will obtain a fourth-degree equation analogous to those of Pierce and Wainstein, in which there furthermore appears a parameter R which may be considered the generalization of the parameter calculated by Derfler. First, therefore, we will assume that if the field in the absence of the beam is derived from an eigenfunction T_m^0 , the current inside the beam equals $J^0 T_m^0$ where J_m^0 can be found from Eqs. 2 and 4, and equals (writing T_m in place of T)

$$J_m^0 = j\omega\epsilon_0 \frac{\omega_p^2}{(j\omega - r_m \mu_0)^2} E_{zm}$$

This does not introduce any very gross error, since, as we

will see, the equation for the calculation of r_m may be written in a variational form with respect to T_m^0 . Then, to find the field throughout the guide section, we rewrite Eq. 4 to include Eq. 7, in the form:

$$\nabla_T^2 T - (K^2 - \Gamma_m^2) T = -J_m^0 J_m^0 I(r - r_0) \quad (8)$$

where $I(r - r_0)$ is a zero function outside the beam and equal to 1 on the inside. Now the second member quantity of Eq. 8 may be developed serially for the cold waves T_n , in the following manner.

$$J_m^0 T_m^0 I(r - r_0) = \sum_n J_n^0 T_n^0 I(r - r_0) \quad (9)$$

by using these waves' property of orthogonality [5]

$$\int_S (E_m \times H_n - E_n \times H_m) \cdot \mathbf{z}_0 dS = N \delta_{mn} \quad (9a)$$

/1007

where $\delta_{m,n}$ is Kroenecker's symbol. Then, also considering the function T which can be developed serially for these waves, one gets ([1], chap. 6).

$$\nabla_T^2 \sum_n A_n T_n^0 - (K^2 - \Gamma_m^2) \sum_n A_n T_n^0 = - \sum_n J_n^0 T_n^0 \quad (10)$$

where the coefficients J_n can be determined using the aforementioned condition of orthogonality. Then, breaking up Eq. 10 into an infinite number of equations for each value of n , one can calculate A_n as a function of J_n , and find, from the vector potential thus obtained, the field $E_2' = E_f$ corresponding to it. Thus

one gets (cf. also [5]).

$$E_f = j \left[\frac{1}{\omega \epsilon_0} T_m + \sum_n \frac{T_n}{\omega^2 - \omega_n^2} Z_{on} \gamma_n T_n \right] \quad (11)$$

where:

$$Z_{on} = \frac{2(E_{zn})^2}{\int_S (E_n \times H_m - E_m \times H_n) \cdot z_0 dS} ; \quad \gamma_n = \int_{S_1} T_m T_n^* dS \quad (11a)$$

where S_1 is the section of the beam and S is the section of the guide in which the waves are propagated. The field E_f thus calculated results from the perturbation of cold waves, to it we add a field E_{sp} due to the modulation of the beam in such a way that the longitudinal field equals

$$E_z = E_f + E_{sp} \quad (12)$$

To calculate E_{spm} the reasoning is completely parallel to that above. Let us consider a sum of space charge waves uncoupled from the synchronous mode. These waves may be precisely the space charge waves of a guide with perfectly conductive walls of a section S geometrically identical to that of the periodic structure. These waves, due to the Coulomb interaction of the electrons, may be considered as the eigensolution of Poisson's equation ([7] p 169 and 200 ff.) Our problem is /1007 to find E_{spm} on the inside of the beam. To do this we observe that on the contour of the latter, S is written (indicating the normal versor on the contour s_1 of the beam) as:

$$\frac{b}{T(s)} \frac{\partial T(b)}{\partial n} - \frac{(K^2 - \Gamma^2)}{j\omega \epsilon_0} b \gamma(\beta_z b) = - \frac{(\beta_z b)^4}{j\omega \epsilon_0 b} \gamma'(\beta_z b) = \text{const.} \quad (13)$$

Actually a guide with perfectly conductive walls does not have poles for $\Gamma = j\beta_e$. Then, applying Green's lemma to two functions T_n and T_m relative to two space charge waves, one gets:

$$\int_{S_1} T_m T_n \left(\frac{\partial T_n}{\partial n} - \frac{\partial T_m}{\partial n} \right) dS = (\kappa_n^2 - \kappa_m^2) \int_{S_1} T_m T_n dS \quad (13a)$$

That is, for the functions found in the approximative manner using Eq. 13, the property of orthogonality equals:

$$\int_{S_1} T_m T_n dS = N_n \delta_{mn} \quad (14)$$

Using this relationship we can repeat the line of reasoning used already with the perturbation of colds axes, writing:

$$J_{zm} = J_m^0 (T_{fm} + T_{spm}) \quad (14a)$$

The significance of the symbols is obvious (in the preceding treatment we set $T_{fm} \approx T_m^0$).

The current is zero outside the beam, thus we can write:

$$J_{spm} = J_m^0 T_{spm} \frac{1}{2} (1 - \epsilon_s) \quad (14b)$$

In this manner we get:

/1009

$$(\kappa_n^2 - \kappa_m^2) T_{spm} = -J_m^0 \sum \frac{\int_{S_1} T_{spm} T_n dS}{\int_{S_1} T_n^2 dS} T_n \quad (15)$$

Analogously to what was done for Eq. 10, remembering.

$$\beta_e^2 \approx |\Gamma_m|^2 \gg \kappa^2 \quad (15b)$$

one finds:

$$E_{spm} = E_{spm}^0 T_{spm} = -\frac{J_m^0}{j\omega\epsilon_0} \sum_n R_n^2 \frac{\int_{S_I} T_{spm} T_n dS}{\int_{S_I} T_n^2 dS} T_n \quad (16)$$

where

$$R_n^2 = \frac{1}{1 - \frac{k_{Tn}^2}{\beta_c^2}} \quad (16a)$$

Then setting

$$\frac{E_{spm}^0}{J_m^0} j\omega\epsilon_0 = -\bar{R}_m^2 \quad (16b)$$

one gets the integral equation in T_{spm} :

$$\bar{R}_m^2 T_{spm}(z) = \int_{S_I} \sum_n \left(R_n^2 \frac{T_{spm}(z) T_n(z)}{\int_{S_I} T_n^2 dS} \right) T_n(z) dS \quad (17)$$

From this, multiplying both sides by T_{spm} and integrating with S_I , one gets the variational expression of $\bar{R}_m^2$ which may /1010 be considered the mean reduction factor for the plasma frequency:

$$\bar{R}_m^2 = \frac{\int_{S_I} \left(\sum_n R_n^2 \frac{\int_{S_I} T_{spm}(z) T_n(z) dS}{\int_{S_I} T_n^2 dS} \right) T_n(z) T_{spm}(z) dS}{\int_{S_I} (T_{spm}(z))^2 dS} \quad (18)$$

However, we have seen that for T_{spm} in the domain S_I the development appearing in the second member of Eq. 15 applies. One can thus write

$$\bar{R}_m^2 = \frac{\sum_n \left[\left(\int_{S_I} T_{spm}(z) T_n(z) dS \right)^2 / \int_{S_I} T_n^2 dS \right] R_n^2}{\sum_n \left(\int_{S_I} T_{spm}(z) T_n(z) dS \right)^2 / \int_{S_I} T_n^2 dS} = \frac{\sum_n f_n^2 R_n^2}{\sum_n f_n^2} \quad (19)$$

To calculate this expression one may consider the field due to modulation of the space charge as being proportional point by point to $T_{fm} \simeq T_{spm}$.

Under this hypothesis one can write

$$E_{zm} = (E_{fm}^* + E_{spm}^*) T_{fm} \simeq (E_{fm}^* - R_m^* \frac{J_m^*}{j\omega\epsilon_0}) T_{fm} \quad (20)$$

Introducing Eq. 20 into Eq. 7 one gets:

$$J_{zm} = j\omega\epsilon_0 \frac{\beta_p^2}{(j\beta_c - \Gamma_m)^2 + \bar{R}^2 \beta_p^2} E_{fm}^* \quad (21)$$

where

$$\beta_p = \frac{\omega_p}{u_0} \quad (21a)$$

Finally, by comparing Eq. 21 with Eq. 11 we get. /1011

$$\frac{(j\beta_c - \Gamma_m)^2 + \bar{R}^2 \beta_p^2}{j\omega\epsilon_0 \beta_p^2} T_m^* = -\frac{1}{j\omega\epsilon_0} T_m^* + \sum_n \frac{\Gamma_n^*}{\Gamma_m^2 - \Gamma_n^2} Z_{on} \psi_n T_n^* \quad (21b)$$

Then, multiplying the preceding by T_m^* and integrating with S_I , one gets an equation for the variational propagation constants in the last eigenfunction. We can now make the usual equations for this type of problem (cf. [7] chap. 10, and [5,6])

$$\begin{aligned} R^2 &= - \frac{\omega\epsilon_0}{\int T_m^* dS} \sum_n \frac{\Gamma_n^*}{\Gamma_m^2 - \Gamma_n^2} Z_{on} (\psi_n)^2 \\ Q_i &= \frac{R^2}{C} \left(\frac{1}{2} \frac{\omega_p}{\omega_c} \right) \\ C &= \sqrt{\frac{Z_m I_0}{4V_0}} \\ Z_m &= Z_m \int T_m^* dS \end{aligned} \quad (21c)$$

where I_0 and V_0 are the continual current and tension of the beam. One thus obtains the fourth-degree equation:

$$\left[(\Gamma_m^0 - j\beta_e)^2 + \bar{R}_m^2 \beta_p^2 + C^2 \Gamma_m^2 4Q \right] (\Gamma_m^2 - \Gamma_m'^2) = 2jC^2 \Gamma_m^2 \beta_e \Gamma_m'^2 \quad (22)$$

In this, in addition to the parameter Q calculated by Pierce and Wainstein, there appears the term due to the space charge waves.

It is now opportune, however, by analogy to Derfler, to define a parameter Q_{tot} as:

$$Q_{tot} = Q + \frac{\bar{R}_m^2}{4C} \left(\frac{\omega_p}{\omega_c} \right)^2 \quad (22a)$$

/1012

In this way the equation takes on the form of Pierce's equation. This makes it possible to calculate the projections and verifications, utilizing the studies already performed by various authors [1,7,8] for a quick solution to Pierce's equation. In the second place, if it is impossible to assume that the electrons all come out of the electron gun at the same velocity, it is necessary to derive a differential equation from Eq. 22 for the function $f(z_1 u_2)$ of the electron density of the phase plane (setting the symbol $\frac{\delta}{\delta_z}$ in place of the quantity ∇_{T_m}) so as to resolve at the same time Boltzmann's equation, which $f(z_1 u_2)$ [sic] must satisfy. This study was performed by D.A. Watkins and H. Rynn [3] for Pierce's equation. The result was that they found a further term (due to the velocity distribution function) to be added to Pierce's parameter Q . Thus one finds that one can define a comprehensive parameter for all three effects examined.

$$Q_{tot} = Q + \frac{\bar{R}_m^2}{4C} \left(\frac{\omega_p}{\omega_c} \right)^2 + \frac{S}{4C} \quad (22b)$$

where for a semi-Maxwell distribution function [3], S equals

$$S = \frac{3}{4} \left(\frac{K T_c}{C V_0} \right) \frac{V}{C^2} \quad (22c)$$

where

K = Boltzmann's constant

T_c = temperature of cathode.

3. Physical significance of the Results

Marcuvits [6] demonstrated that where the modes of the cold guide are orthogonal with respect to those of a guide suitably /1013 conjugate to it, the modes of the electron guide are orthogonal with respect to the modes of the electron guide conjugate to it and are obtained from the cold conjugate guide and the same electron beam. In the case of a periodic structure not containing dielectrics with tensorial constants, the conjugate guide coincides with the same periodic structure and the property of orthogonality takes on the form

$$\int_S (\underline{E}_n \times \underline{H}_{-m} - \underline{E}_{-m} \times \underline{H}_n) \underline{Z}_0 dS + \int_S (V_n \underline{J}_m + V_m \underline{J}_n) dS = N_n \delta_{m,n} \quad (23)$$

where

$$V = \frac{u_0 u_1}{\gamma} \quad (24)$$

with u_1 being the alternative component of the electron velocity.

From this property one can see that if one perturbs the cold solution consisting of fields for which the orthogonality relationships applies

$$\int_S (\underline{E}_n \times \underline{H}_{-m} - \underline{E}_{-m} \times \underline{H}_n) \underline{Z}_0 dS = N_n \delta_{m,n} \quad (25)$$

then these fields are coupled by way of the current they excite in the beam. The parameter Q defined by Pierce and Wainstein's equations in fact contains a sum of terms which can be interpreted as the mutual coupling impedances of the various modes across the beam. However, it has already been observed that the presence of the beam introduces an ensemble of space charge waves. These also are coupled to the synchronous wave. The parameter $\bar{R}_m$ we defined actually also contains a sum of terms which may be considered as being due to mutual coupling impedances between the synchronous modes and the space charge waves. For this very reason, the field due to serial beam modulation for the space charge waves in a guide with perfectly conductive walls was developed. This also explains why the parameter Q_{tot} was /1014 obtained as the sum of two terms. The first results from the slow wave corresponding to imaginary eigenvalues. In other words, the parameter Q expresses the coupling of the synchronous wave with the other waves supported by the periodic structure, and the parameter $\bar{R}_m$ expresses the coupling of this same wave with those waves supported by the beam.

Note that by substituting the value $T_{sp} = I_0(\beta e r)$ in the expression for $\bar{R}_m$, (in the case of cylindrical symmetry) one obtains for f_n (Eq. 19)

$$f_n = \frac{q_n / \beta e b}{1 + \left(\frac{q_n}{\beta e b}\right)^2} \frac{1}{\sqrt{1 + \left(\frac{q_n}{H}\right)^2}} I_0(\beta e b) \left[1 + \frac{\beta e b}{H} \frac{I_1(\beta e b)}{I_0(\beta e b)} \right] \quad (26)$$

where

$$q_n^2 = |K_{Tn}|^2 b^2 \quad (27)$$

and

$$H = q_n \frac{J_1(q_n)}{J_0(q_n)} = -\beta e b \frac{I_1(\beta e b) K_0(\beta e Q) + K_1(\beta e b) I_0(\beta e Q)}{I_0(\beta e b) K_0(\beta e Q) + K_0(\beta e b) I_0(\beta e Q)} \quad (28)$$

The expression for f_n concides except for one independent constant with the formula (of the same type as Eq 19) calculated by Derfler.

$$f_n^D = \frac{q_n / \beta e b}{1 + \left(\frac{q_n}{\beta e b}\right)^2} \frac{1}{\sqrt{1 + \left(\frac{q_n}{H}\right)^2}} \frac{I_0(\beta e b)}{I_0(\beta e Q)} \left[1 + \frac{\beta e b}{H} \frac{I_1(\beta e Q)}{I_0(\beta e Q)} \right] \quad (29)$$

N.B. In these formulas b represents the radius of the circumference which defines the beam, and a the radius which defines (in the case of cylindrical symmetry) the circle corresponding to the section S .

1. Pierce, J R., Traveling Wave Tubes, Van Nostrand, 1950, chap. 6 and 7.
2. Birdsall, C.K., and J R. Whinnery, "Waves in electron streams with general admittance walls, J. Appl. Phys., 314-23 (March 1953).
3. Watkins, D.A., and N. Rynn "Effect of velocity distribution on traveling wave tube gain", J. Appl. Phys. 1375-9 (November 1954).
4. Derfler, H., "Plasma waves in finite electron beams and their interaction with field waves," International Congress on Microwave Tubes, ed. Elsevier, Paris, 1956, pp. 326-1958.
5. Wainstein, L A., "Electronic waves in delay lines," International Congress on Microwave Tubes, ed. Elsevier, Paris, 1956, pp. 432 ff.
6. Marcuvitz, Nathan, "General electronic waveguides," Proceedings of the Symposium on Electronic Waveguides, New York, April 1958, pp. 63-68.
7. Hutter, R.G.E , Beam and Wave Electronics in Microwave Tubes , Van Nostrand, 1960, chaps 6-10.